## Lecture 15

## More on Interesting Physical Phenomena

Though simple that it looks, embedded in the TM Fresnel reflection coefficient are a few more interesting physical phenomena. These are the phenomena of Brewster's angle [96, 97] and the phenomena of surface plasmon resonance, or polariton [98, 99].

### 15.1 More on Interesting Physical Phenomena, Homomorphism, Plane Waves, Transmission Lines

We will continue with understanding some interesting phenomena associated with the singleinterface problem.

### 15.1.1 Brewster Angle



Figure 15.1: A figure showing a plane wave being reflected and transmitted at the Brewster's angle. In Region $t$, the polarization current or dipoles are all pointing in the $\mathbf{k}_{r}$ direction, and hence, there is no radiation in that direction (courtesy of J.A. Kong, EM Wave Theory [31]).

Brewster angle was discovered in 1815 [96, 97]. Furthermore, most materials at optical frequencies have $\varepsilon_{2} \neq \varepsilon_{1}$, but $\mu_{2} \approx \mu_{1}$. In other words, it is hard to obtain magnetic materials at optical frequencies. Therefore, the TM polarization for light behaves differently from TE polarization. Hence, we shall focus on the reflection and transmission of the TM polarization of light, and we reproduce the previously derived TM reflection coefficient here:

$$
\begin{equation*}
R^{T M}=\left(\frac{\beta_{1 z}}{\varepsilon_{1}}-\frac{\beta_{2 z}}{\varepsilon_{2}}\right) /\left(\frac{\beta_{1 z}}{\varepsilon_{1}}+\frac{\beta_{2 z}}{\varepsilon_{2}}\right) \tag{15.1.1}
\end{equation*}
$$

The transmission coefficient is easily gotten by the formula $T^{T M}=1+R^{T M}$. Observe that for $R^{T M}$, it is possible that $R^{T M}=0$ if

$$
\begin{equation*}
\varepsilon_{2} \beta_{1 z}=\varepsilon_{1} \beta_{2 z} \tag{15.1.2}
\end{equation*}
$$

Squaring the above, making the note that $\beta_{i z}=\sqrt{\beta_{i}^{2}-\beta_{x}^{2}}$, one gets

$$
\begin{equation*}
\varepsilon_{2}^{2}\left(\beta_{1}^{2}-\beta_{x}^{2}\right)=\varepsilon_{1}^{2}\left(\beta_{2}^{2}-\beta_{x}^{2}\right) \tag{15.1.3}
\end{equation*}
$$

Solving the above, assuming $\mu_{1}=\mu_{2}=\mu$, gives

$$
\begin{equation*}
\beta_{x}=\omega \sqrt{\mu} \sqrt{\frac{\varepsilon_{1} \varepsilon_{2}}{\varepsilon_{1}+\varepsilon_{2}}}=\beta_{1} \sin \theta_{1}=\beta_{2} \sin \theta_{2} \tag{15.1.4}
\end{equation*}
$$

The latter two equations come from phase matching at the interface. Therefore,

$$
\begin{equation*}
\sin \theta_{1}=\sqrt{\frac{\varepsilon_{2}}{\varepsilon_{1}+\varepsilon_{2}}}, \quad \sin \theta_{2}=\sqrt{\frac{\varepsilon_{1}}{\varepsilon_{1}+\varepsilon_{2}}} \tag{15.1.5}
\end{equation*}
$$

or that

$$
\begin{equation*}
\sin ^{2} \theta_{1}+\sin ^{2} \theta_{2}=1 \tag{15.1.6}
\end{equation*}
$$

Then, assuming that $\theta_{1}$ and $\theta_{2}$ are less than $\pi / 2$, and using the identity that $\cos ^{2} \theta_{1}+\sin ^{2} \theta_{1}=$ 1 , then it can be shown that

$$
\begin{equation*}
\sin \theta_{2}=\cos \theta_{1} \tag{15.1.7}
\end{equation*}
$$

or that

$$
\begin{equation*}
\theta_{1}+\theta_{2}=\pi / 2 \tag{15.1.8}
\end{equation*}
$$

This is used to explain why at Brewster angle, no light is reflected back to Region 1. Figure 15.1 shows that the induced polarization dipoles in Region 2 always have their axes aligned in the direction of reflected wave. A dipole does not radiate along its axis, which can be verified heuristically by field sketch and looking at the Poynting vector. Therefore, these induced dipoles in Region 2 do not radiate in the direction of the reflected wave. Notice that when the contrast is very weak meaning that $\varepsilon_{1} \cong \varepsilon_{2}$, then $\theta_{1} \cong \theta_{2} \cong \pi / 4$, and (15.1.8) is satisfied.

Because of the Brewster angle effect for TM polarization when $\varepsilon_{2} \neq \varepsilon_{1},\left|R^{T M}\right|$ has to go through a null when $\theta_{i}=\theta_{b}$. Therefore, $\left|R^{T M}\right| \leq\left|R^{T E}\right|$ as shown in Figure 15.2. Then when a randomly polarized light is incident on a surface, the polarization where the electric field is parallel to the surface (TE polarization) is reflected more than the polarization where the magnetic field is parallel to the surface (TM polarization). This phenomenon is used to design sun glasses to reduce road glare for drivers. For light reflected off a road surface, they are predominantly horizontally polarized with respect to the surface of the road. When sun glasses are made with vertical polarizers, they will filter out and mitigate the reflected rays from the road surface to reduce road glare. This phenomenon can also be used to improve the quality of photography by using a polarizer filter as shown in Figure 15.3.


Figure 15.2: Because $\left|R^{T M}\right|$ has to through a null when $\theta_{i}=\theta_{b}$, therefore, $\left|R^{T M}\right| \leq\left|R^{T E}\right|$ for all $\theta_{i}$ as shown above.


Figure 15.3: Because the TM and TE lights will be reflected differently, polarizer filter can produce remarkable effects on the quality of the photograph by reducing glare [97].

### 15.1.2 Surface Plasmon Polariton

Surface plasmon polariton occurs for the same mathematical reason for the Brewster angle effect but the physical mechanism is quite different. Many papers and textbooks will introduce this phenomenon from a different angle. But here, we will introduce it from the Fresnel reflection coefficient for the TM waves.

The reflection coefficient $R^{T M}$ can become infinite if $\varepsilon_{2}<0$, which is possible in a plasma medium. In this case, the criterion for the denominator to be zero is

$$
\begin{equation*}
-\varepsilon_{2} \beta_{1 z}=\varepsilon_{1} \beta_{2 z} \tag{15.1.9}
\end{equation*}
$$

When the above is satisfied, $R^{T M}$ becomes infinite. This implies that a reflected wave exists when there is no incident wave. Or $H_{\mathrm{ref}}=H_{\mathrm{inc}} R^{T M}$, and when $R^{T M}=\infty, H_{\mathrm{inc}}$ can be
zero, and $H_{\text {ref }}$ can assume any value. ${ }^{1}$ Hence, there is a plasmonic resonance or guided mode existing at the interface without the presence of an incident wave. It is a self-sustaining wave propagating in the $x$ direction, and hence, is a guided mode propagating in the $x$ direction.

Solving (15.1.9) after squaring it, as in the Brewster angle case, yields

$$
\begin{equation*}
\beta_{x}=\omega \sqrt{\mu} \sqrt{\frac{\varepsilon_{1} \varepsilon_{2}}{\varepsilon_{1}+\varepsilon_{2}}} \tag{15.1.10}
\end{equation*}
$$

This is the same equation for the Brewster angle except now that $\varepsilon_{2}$ is negative. Even if $\varepsilon_{2}<0$, but $\varepsilon_{1}+\varepsilon_{2}<0$ is still possible so that the expression under the square root sign (15.1.10) is positive. Thus, $\beta_{x}$ can be pure real. The corresponding $\beta_{1 z}$ and $\beta_{2 z}$ in (15.1.9) can be pure imaginary, and (15.1.9) can still be satisfied.

This corresponds to a guided wave propagating in the $x$ direction. When this happens,

Since $\varepsilon_{2}<0, \varepsilon_{2} /\left(\varepsilon_{1}+\varepsilon_{2}\right)>1$, then $\beta_{1 z}$ becomes pure imaginary. Moreover, $\beta_{2 z}=\sqrt{\beta_{2}{ }^{2}-\beta_{x}{ }^{2}}$ and $\beta_{2}{ }^{2}<0$ making $\beta_{2 z}$ becomes even a larger imaginary number. This corresponds to a trapped wave (or a bound state) at the interface. The wave decays exponentially in both directions away from the interface and they are evanescent waves. This mode is shown in Figure 15.4, and is the only case in electromagnetics where a single interface can guide a surface wave, while such phenomenon abounds for elastic waves.

When one operates close to the resonance of the mode so that the denominator in (15.1.10) is almost zero, then $\beta_{x}$ can be very large. The wavelength becomes very short in this case, and since $\beta_{i z}=\sqrt{\beta_{i}^{2}-\beta_{x}^{2}}$, then $\beta_{1 z}$ and $\beta_{2 z}$ become even larger imaginary numbers. Hence, the mode becomes tightly confined or bound to the interface, making the confinement of the mode very tight. This evanescent wave is much more rapidly decaying than that offered by the total internal reflection. It portends use in tightly packed optical components, and has caused some excitement in the optics community.

[^0]

Figure 15.4: Figure showing a surface plasmonic mode propagating at an air-plasma interface. As in all resonant systems, a resonant mode entails the exchange of energies. In the case of surface plasmonic resonance, the energy is exchanged between the kinetic energy of the electrons and the energy store in the electic field (courtesy of Wikipedia [100]).

### 15.2 Homomorphism of Uniform Plane Waves and Transmission Lines Equations

It turns out that the plane waves through layered medium can be mapped into the multisection transmission line problem due to mathematical homomorphism between the two problems. Hence, we can kill two birds with one stone: apply all the transmission line techniques and equations that we have learnt to solve for the solutions of waves through layered medium problems. ${ }^{2}$

For uniform plane waves, since they are proportional to $\exp (-j \boldsymbol{\beta} \cdot \mathbf{r})$, we know that with $\nabla \rightarrow-j \boldsymbol{\beta}$, Maxwell's equations becomes

$$
\begin{array}{r}
\boldsymbol{\beta} \times \mathbf{E}=\omega \mu \mathbf{H} \\
\boldsymbol{\beta} \times \mathbf{H}=-\omega \varepsilon \mathbf{E} \tag{15.2.2}
\end{array}
$$

for a general isotropic homogeneous medium. We will specialize these equations for different polarizations.

### 15.2.1 TE or $\mathrm{TE}_{z}$ Waves

For this, one assumes a TE wave traveling in the $z$ direction with electric field polarized in the $y$ direction, or $\mathbf{E}=\hat{y} E_{y}, \mathbf{H}=\hat{x} H_{x}+\hat{z} H_{z}$, then we have from (15.2.1)

$$
\begin{align*}
& \beta_{z} E_{y}=-\omega \mu H_{x}  \tag{15.2.3}\\
& \beta_{x} E_{y}=\omega \mu H_{z} \tag{15.2.4}
\end{align*}
$$

[^1]From (15.2.2), we have

$$
\begin{equation*}
\beta_{z} H_{x}-\beta_{x} H_{z}=-\omega \varepsilon E_{y} \tag{15.2.5}
\end{equation*}
$$

Then, expressing $H_{z}$ in terms of $E_{y}$ from (15.2.4), we can show from (15.2.5) that

$$
\begin{align*}
\beta_{z} H_{x} & =-\omega \varepsilon E_{y}+\beta_{x} H_{z}=-\omega \varepsilon E_{y}+\frac{\beta_{x}^{2}}{\omega \mu} E_{y} \\
& =-\omega \varepsilon\left(1-\beta_{x}^{2} / \beta^{2}\right) E_{y}=-\omega \varepsilon \cos ^{2} \theta E_{y} \tag{15.2.6}
\end{align*}
$$

where $\beta_{x}=\beta \sin \theta$ has been used.
Eqns. (15.2.3) and (15.2.6) can be written to look like the telegrapher's equations by letting $-j \beta_{z} \rightarrow d / d z$ to get

$$
\begin{align*}
\frac{d}{d z} E_{y} & =j \omega \mu H_{x}  \tag{15.2.7}\\
\frac{d}{d z} H_{x} & =j \omega \varepsilon \cos ^{2} \theta E_{y} \tag{15.2.8}
\end{align*}
$$

If we let $E_{y} \rightarrow V, H_{x} \rightarrow-I, \mu \rightarrow L, \varepsilon \cos ^{2} \theta \rightarrow C$, the above is exactly analogous to the telegrapher's equations. The equivalent characteristic impedance of these equations above is then

$$
\begin{equation*}
Z_{0}=\sqrt{\frac{L}{C}}=\sqrt{\frac{\mu}{\varepsilon}} \frac{1}{\cos \theta}=\sqrt{\frac{\mu}{\varepsilon}} \frac{\beta}{\beta_{z}}=\frac{\omega \mu}{\beta_{z}} \tag{15.2.9}
\end{equation*}
$$

The above is the wave impedance for a propagating plane wave with propagation direction or the $\boldsymbol{\beta}$ inclined with an angle $\theta$ respect to the $z$ axis. When $\theta=0$, the wave impedance becomes the intrinsic impedance of space.

A two region, single-interface reflection problem can then be mathematically mapped to a single-junction two-transmission-line problem discussed in Section 13.1.1. The equivalent characteristic impedances of these two regions are then

$$
\begin{equation*}
Z_{01}=\frac{\omega \mu_{1}}{\beta_{1 z}}, \quad Z_{02}=\frac{\omega \mu_{2}}{\beta_{2 z}} \tag{15.2.10}
\end{equation*}
$$

We can use the above to find $\Gamma_{12}$ as given by

$$
\begin{equation*}
\Gamma_{12}=\frac{Z_{02}-Z_{01}}{Z_{02}+Z_{01}}=\frac{\left(\mu_{2} / \beta_{2 z}\right)-\left(\mu_{1} / \beta_{1 z}\right)}{\left(\mu_{2} / \beta_{2 z}\right)+\left(\mu_{1} / \beta_{1 z}\right)} \tag{15.2.11}
\end{equation*}
$$

The above is the same as the Fresnel reflection coefficient found earlier for TE waves or $R^{T E}$ after some simple re-arrangement.

Assuming that we have a single junction transmission line, one can define a transmission coefficient given by

$$
\begin{equation*}
T_{12}=1+\Gamma_{12}=\frac{2 Z_{02}}{Z_{02}+Z_{01}}=\frac{2\left(\mu_{2} / \beta_{2 z}\right)}{\left(\mu_{2} / \beta_{2 z}\right)+\left(\mu_{1} / \beta_{1 z}\right)} \tag{15.2.12}
\end{equation*}
$$

The above is similar to the continuity of the voltage across the junction, which is the same as the continuity of the tangential electric field across the interface. It is also the same as the Fresnel transmission coefficient $T^{T E}$.

### 15.2.2 TM or $\mathrm{TM}_{z}$ Waves

For the TM polarization, by invoking duality principle, the corresponding equations are, from (15.2.7) and (15.2.8),

$$
\begin{align*}
\frac{d}{d z} H_{y} & =-j \omega \varepsilon E_{x}  \tag{15.2.13}\\
\frac{d}{d z} E_{x} & =-j \omega \mu \cos ^{2} \theta H_{y} \tag{15.2.14}
\end{align*}
$$

Just for consistency of units, since electric field is in $\mathrm{Vm}^{-1}$, and magnetic field is in $\mathrm{Am}^{-1}$ we may chose the following map to convert the above into the telegrapher's equations, viz;

$$
\begin{equation*}
E_{y} \rightarrow V, \quad H_{y} \rightarrow I, \quad \mu \cos ^{2} \theta \rightarrow L, \quad \varepsilon \rightarrow C \tag{15.2.15}
\end{equation*}
$$

Then, the equivalent characteristic impedance is now

$$
\begin{equation*}
Z_{0}=\sqrt{\frac{L}{C}}=\sqrt{\frac{\mu}{\varepsilon}} \cos \theta=\sqrt{\frac{\mu}{\varepsilon}} \frac{\beta_{z}}{\beta}=\frac{\beta_{z}}{\omega \varepsilon} \tag{15.2.16}
\end{equation*}
$$

The above is also termed the wave impedance of a TM propagating wave making an inclined angle $\theta$ with respect to the $z$ axis. Notice again that this wave impedance becomes the intrinsic impedance of space when $\theta=0$.

Now, using the reflection coefficient for a single-junction transmission line, and the appropriate characteristic impedances for the two lines as given in (15.2.16), we arrive at

$$
\begin{equation*}
\Gamma_{12}=\frac{\left(\beta_{2 z} / \varepsilon_{2}\right)-\left(\beta_{1 z} / \varepsilon_{1}\right)}{\left(\beta_{2 z} / \varepsilon_{2}\right)+\left(\beta_{1 z} / \varepsilon_{1}\right)} \tag{15.2.17}
\end{equation*}
$$

Notice that (15.2.17) has a sign difference from the definition of $R^{T M}$ derived earlier in the last lecture. The reason is that $R^{T M}$ is for the reflection coefficient of magnetic field while $\Gamma_{12}$ above is for the reflection coefficient of the voltage or the electric field. This difference is also seen in the definition for transmission coefficients. ${ }^{3}$ A voltage transmission coefficient can be defined to be

$$
\begin{equation*}
T_{12}=1+\Gamma_{12}=\frac{2\left(\beta_{2 z} / \varepsilon_{2}\right)}{\left(\beta_{2 z} / \varepsilon_{2}\right)+\left(\beta_{1 z} / \varepsilon_{1}\right)} \tag{15.2.18}
\end{equation*}
$$

But this will be the transmission coefficient for the voltage, which is not the same as $T^{T M}$ which is the transmission coefficient for the magnetic field or the current. Different textbooks may define different transmission coefficients for this polarization.

[^2]
[^0]:    ${ }^{1}$ This is often encountered in a resonance system like an LC tank circuit. Current flows in the tank circuit despite the absence of an exciting voltage.

[^1]:    ${ }^{2}$ This treatment is not found elsewhere, and is peculiar to these lecture notes.

[^2]:    ${ }^{3}$ This is often the source of confusion for these reflection and transmission coefficients.

